Abfraction: 3D analysis by means of the finite element method

Allahyar Geramy, DDS, MScD1/Farahnaz Sharafoddin, DDS, MScD2

Objective: Tooth deflections under functional loads are considered to be the etiologic factor of noncarious cervical lesions. There are several studies on the materials used to restore these lesions; however, there are few discussing this phenomenon's etiology from a biomechanic point of view. This study was undertaken to evaluate tooth behavior when forces were applied from different directions. Method and materials: A 3D finite element model of a maxillary central incisor was designed. A distributed force of 1.5 N was applied on the palatal side of the crown in five stages, with varying directions progressing from tipping to intrusion. Two separate approaches (displacement and stress) were considered to evaluate the cervical area from a stress perspective. Results: The displacement approach resulted in a curved path when compared to a straight line connecting the apical and incisal areas. The maximum deflections were in the cementoenamel junction area. The same area was shown to undergo the maximum of von Mises stress and stress intensity. Patterns of the von Mises stress when evaluated in a mesiodistal direction were in complete agreement with the shape of the cervical lesions (except for the application of the intrusive force, which rules out its effect in producing such lesions). Conclusion: Force applications, except for intrusive force, can produce increases in the von Mises stress and tooth deflections that can answer the question of the etiology of noncarious cervical lesions. The highest amounts of deflection and von Mises stress were produced by the 45-degree force application. (Quintessence Int 2003;34:526-533)

Key words: abfraction, finite element method, force application, functional loads, stress

CLINICAL RELEVANCE: A noncarious cervical lesion is a challenging area for restorative dentists, researchers who work on new materials, and biomechanics experts. Its etiology can be discussed somewhat accurately but cannot be prevented in many cases. Applying new materials in this region is questionable due to acting forces. Long-term survival of materials used to restore such a lesion should be assessed.

At the same time of moving, teeth flex under various loads. This is an important point in operative dentistry, prosthodontics, and implantology, though it is ignored in orthodontic therapies. This type of reaction to external loads has been interpreted to be the cause of some cervical lesions without signs of caries.

Noncarious cervical lesions are characterized by the loss of hard tissue at the cementoenamel junction.¹ Traditionally, it has been assumed to be due to the effects of abrasion and/or erosion. More recently, researchers have stated a new theory that relates these lesions to cuspal flexure. 1-3 Tooth flexure has been described as a lateral or axial bending under occlusal loading. Tooth flexure produces tensile or compressive strain, causing a disruption of the bonds between hydroxyapatite crystals, leading to the formation of cracks in the enamel and the eventual loss of enamel and underlying dentin. 1-3-6

Grippo⁷ coined the term abfraction to distinguish this type of cervical lesion associated with cuspal flexure. The term dental abfraction tries to show the presence of tooth fatigue, flexure, and deformation through biomechanic loading of teeth, primarily at the cervical regions of the dentition.⁴⁷ Xhonga⁸ found a significantly higher prevalence of these lesions in patients with bruxism.

According to Burke et al, 9 there is evidence to support the cuspal flexure theory in the formation of cervical lesions: (1) Lesions occur in teeth subjected to lateral loads, but the adjacent teeth not undergoing the load remain unaffected; (2) lesions are rarely seen in the lingual side of teeth; and (3) lesions may occur subgingivally, which would not be the case for erosion or abrasion.

¹Assistant Professor, Department of Orthodontics, Shiraz School of Dental Medicine, Shiraz, Iran.

²Assistant Professor, Department of Operative Dentistry, Shiraz School of Dental Medicine, Shiraz, Iran.

Reprint requests: Dr Allahyar Geramy, Department of Orthodontics, Shiraz School of Dental Medicine, PO Box 71345-1836, Shiraz, Iran. E-mail: gueramya@yahoo.com

The concept of occlusally generated stresses is appealing as it can explain the morphology and location of these wedge-shaped lesions. Reports show that deformations due to occlusal loads could produce a tensile and compressive stress in the cervical region. According to Lee and Eakle, to these tensile stresses are known as the primary etiologic factor of noncarious cervical lesions.

In complicated structures, it is difficult to achieve an accurate analytic solution. Numeric methods, such as the finite element method of analysis (FEA), can be considered a practical approach. Finite element analysis divides the problem domains into a collection of smaller parts (elements). An overall approximated solution to the original problem is determined. In this method, solutions for each element are combined to obtain a solution to the whole body.¹³ Among various methods of assessing deformations produced in different structures, the FEA has proven its efficiency in many ways, from the normal situations concerning the nature of tooth movement under orthodontic loads.¹² to special situations like alveolar bone loss, ^{13,8} extraoral force systems, ¹⁵ and many other fields.

In spite of the presence of various articles dealing with different materials, their applications, advantages, and disadvantages, there are few studies dealing with the etiology of these lesions. This study was undertaken to evaluate the cervical area of a tooth under loads from displacement and stress perspectives.

METHOD AND MATERIALS

A three-dimensional (3D) finite element model (FEM) of a maxillary central incisor was designed. The model consisted of 37,884 nodes and 32,768 elements based on Ash's dental anatomy,33 with minor modifications to obtain the best shape (Fig 1). A 3D brick, isoparametric, octahedral element was chosen to construct the model. The model contained the maxillary central incisor (its crown covered with enamel), its PDL, and spongy and cortical bone (Fig 2). Cementum is a very thin layer and has the same physical properties as dentin: therefore, it seemed unnecessary to define it as a separate layer from the dentin. Each section was given 48 external nodes to enable appropriate modeling. The root was split into 15 levels of varying vertical heights (see Fig 1). According to Coolidge,34 the PDL is of varying thicknesses in vivo (Table 1) and has been thought to make the model more precise and realistic.

Due to technical reasons, the applied force of 1.5 N was divided into 72 small point forces. The points of force application were parallel to the incisal edge, on the palatal side. The direction of the palatolabial forces ranged between tipping (0 degrees relative to

the horizontal line), 22.5, 45, and 65 degrees relative to the horizontal line, and 90 degrees relative to the same line (intrusion).

The boundary condition is an important factor in the FEM, reflecting the manner of movements occurring at the nodes and their relationships. All the nodes at the base of the model were fixed so not to move when subjected to force systems. The analyses were performed on a Pentium III personal computer (ANSYS Version 5.4). Poisson's ratio is the strain in the lateral direction to that in the axial direction when an object is subjected to tensile loading, which increases the length of the object in the direction of the load and decreases the lateral dimensions of the object that are perpendicular to the load. According to experiments 35 this ratio lies between 0.25 and 0.35 for most of the materials. The highest value for this ratio is 0.50 and shows lack of any volume change of the body while deformation occurs. In other words, any axial deformation will be followed by a lateral deformation. In the present study, the Poisson's ratio of the PDL was assumed to be 0.49, which explains its biologic characteristics rather accurately (Table 2).

Symmetric force applications to the tooth's long axis prevented any rotation tendency.

Two separate approaches were considered for evaluations: (1) displacement; and (2) stresses.

Output data of the approaches were derived along two paths defined by the nodes of the most prominent part of the labial and palatal sides of the tooth. The path was from the incisal edge down to the apical area. In the last phase of the analysis, another path was defined mesiodistally in the cervical area to assess the stress situation of that region.

The displacements of the nodes along the path were compared with a straight line connecting the incisal edge to the apical area. In this way, any disproportion produced in the displacement of the nodes due to deformation was made clear. The distance formed between the path and the straight line was calculated at the CEJ area as a criterion for the degree of tooth deformation.

Among the criteria used to evaluate the structures under loading to judge the stress state at certain points, was the von Mises stress

$$\sigma_{e} = (\frac{1}{2} \left[(\sigma_{1} - \sigma_{2})^{2} + (\sigma_{2} - \sigma_{3})^{2} + (\sigma_{3} - \sigma_{1})^{2} \right])^{1/2}$$

and the stress intensity

$$\sigma_1 = \max \left[|\sigma_1 - \sigma_2|, |\sigma_2 - \sigma_3|, |\sigma_3 - \sigma_1| \right].$$

The aforementioned criteria were traced in the path to show the quality of their changes. The last assessment was to find the von Mises pattern of the cervical area in a mesiodistal direction along the second path.

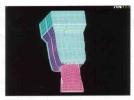


Fig 1 Three-dimensional model of a maxillary central incisor.

Fig 2 (right) The different materials used in

0.22

0.24

0.20

the model. TABLE 1 Geometry of the PDL widths according to Coolidge34 (mm) Distance from the Distal Lingual Mesial Labial alveolar crest 13.0 0.25 0.25 0.22 0.25 10.5 0.18 0.22 0.20 0.22 0.20 0.20 8.0 0.15 0.17 0.18 0.14 0.18 0.16 6.5 5.0 0.15 0.20 0.20

0.22

0.24

0.18

0.19

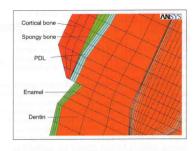
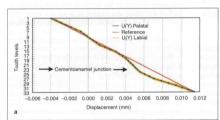


TABLE 2 Mechanical properties of the structural elements of the study		
Material	Young's modulus (N/mm²)	Poisson's ratio
Cortical bone	3.40 × 10 ⁴	0.26
Spongy bone	1.37 × 10 ⁴	0.38
PDL	6.67 × 10 ⁻¹	0.49
Dentin	1.80 × 10 ⁴	0.31
Enamel	8.40 × 10 ⁴	0.33



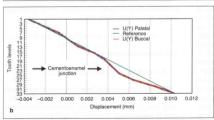


Fig 3 Displacement of the labial and palatal nodes in the direction of the applied force (1.5 N) compared to a straight line connecting the incisal and apical areas: (a) Tipping force application; (c) (facing page) 45-degree force application; (c) (facing page) 45-degree force application; (d) (facing page) 64-degree application; (d) (facing page) 65-degree force application; (d) (facing page) 61-degree force application; and (e) (facing page) intrusive force application; and (e) (facing page) intrusive force application (90 degrees).

25

0.0

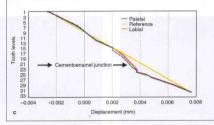
RESULTS

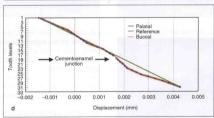
The output data were divided into two main groups according to displacement and stress.

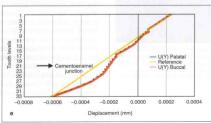
Displacement

Output data for displacement in the palatal and labial sides of the tooth are the same, showing the reliability of the model presented. Displacement results showed some irregularities in the cervical area compared to a straight line passing from the incisal and apical area. Simple

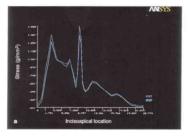
analytic geometric rules were employed to evaluate the output data to find out whether or not they were located in a straight line. At first assessment, the difference between the findings of cervical area displacement and the reference line was calculated. Figures 3a to 3e show the behavior of the tooth in different load cases. The decreases found ranged between 2% in intrusion and 13% in 45-degree force application, with a mean value of 8.11% from the reference line. The patterns of the tooth behavior were almost the same in different load cases except for the intrusion force application.

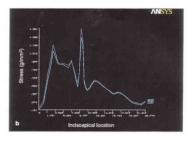


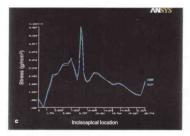


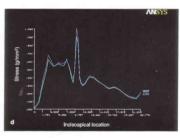


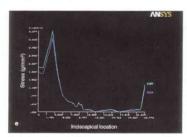
Quintessence International 529











Although the highest amount of deflection was located a few tenths of a millimeter incisal to the CEJ, this area is the weakest and the most susceptible to hard tissue loss.

Fig 4 von Misses stress and stress intensity assessment of the nodes along the labial path: (a) Tipping force application (0 degrees): (b) 22.5-degree force application; (c) 45-degree force application; (d) 56-degree force application; (d) 96-degree force application; (d) 90-degree): SINT = stress intensity, SEQV = von Misses stress.

Stress

Among the criteria used to evaluate a structure from the stress perspective is the von Mises stress and stress intensity. To the best of the authors' knowledge, there is not a maximum bearable stress reported for living tissues. In the present study, output data for the aforementioned criteria are depicted in Figs 4a to 4e. The results show the maximum stress intensity in the cervical area except for the intrusion movement. These figures show that the cervical region was the area of some deformities, exhibited by their displacement in comparison with the straight line and also the area of maximum von Mises stress and stress intensity.

530 Volume 34, Number 7, 2003

DISCUSSION

Any type of stress (tensile, compressive, or shearing), when sufficient in magnitude, can inflict damage on tooth structure. ^{36,37} It is known that lateral force acting on a tooth at the fulcrum creates tension and compression of equal magnitudes on both sides. ³⁶ Tooth structure, particularly the enamel, has a far greater compressive strength than tensile strength. ³⁸ Lambrechts et al³⁹ reported frequent findings of enamel cracks at the cervical enamel under tensile stress. Stereomicroscopic studies, ³⁹ on the other hand, clearly demonstrated evidence of hydroxyapatite crystal disruptions caused by the stress.

Although tensile stress is the major etiologic factor in cervical lesions, it is not to be miscomprehended that all cervical lesions are caused by this stress or that tensile stress is the only factor involved. Stress-induced and abrasion lesions may share a similar morphologic feature. § A relationship between bruxism and dental erosion has been suggested by Xhonga. § It is estimated, in a group presenting wedge-shaped cervical lesions, that 97% of the population under study had parafunctional disorders. § Recent finite element studies \$^{14}\$ Recent finite element studies \$^{14}\$ Respectively. Which is in complete agreement with the findings of the present study.

Several force vectors may act simultaneously on living tissues in a 3D space. It is not appropriate to analyze one plane, while ignoring the other planes because the structure is not symmetric. Based on these facts, two-dimensional (2D) models cannot represent the real situation of a 3D body. In this way, 2D models like those of Takahashi et al⁴⁴ are not expected to show real situations well.

PDL is the most important tissue in the evaluation of any tooth movement. Its role cannot be ignored while trying to achieve a real situation. Rubin et al⁴⁵ tried to analyze the stress distribution in a human mandibular first molar, without modeling the PDL. Although using a 5D model is superior to a 2D model, ignoring PDL can influence results seriously. The model presented in the present study is as similar as possible to the real situation described earlier.

The presence of large values of the strains in the enamel adjacent to the CEJ is explained with the following reasons: (1) It is thinner than the other regions; (2) the enamel rod arrangement is less intertwined near the CEJ than in other regions; and (3) the weaker bond between the enamel and the dentin in the cervical area also may contribute to the occurrence of high strains in the enamel. The tight bond of

the dentinoenamel junction enables the natural tooth to distribute stress into the more elastic dentin in order to minimize the damage from the local stresses on the enamel that result from occlusal contacts. ⁴⁷ Evaluating the von Mises stress of the cervical area in a mesiodistal direction revealed an almost similar pattern in all force directions except for the intrusive force application (Figs 5a to 5c).

Braem et al 39 described the development process of the stress-induced lesions from the initial cracking stage of the outer cervical enamel to the subsequent advancement of the destructive process in the dentin.

A close study of these figures can reveal some important points that can confirm some clinical findings and are in complete agreement with Burke et al.³⁹

- The patterns are the same as and similar with the overall shape of the lesions mesiodistally.
- In spite of the presence of higher stresses in the crown in comparison with the CEJ, the enamel rods are thinner in the CEJ, and the lesions start from this area.
- It can be assumed that once the bond between enamel and dentin starts to disrupt, the lesion continues to develop due to the presence of higher stress values in the incisal part of the CEJ.
- High amounts of stress in the first layer of the crown can be the reason for restorative material failure in this area.
- Curve shapes of the intrusive movement show that this kind of force does not have any effect on the etiology of these lesions.

CONCLUSION

Force application causes an elastic deformation in the teeth that was clearly shown by the FEA. The simplest interpretation of less displacement of the nodes in the CEJ and the adjacent areas is that the tooth containing these nodes had been flexed in this area, providing less displacement in comparison with the reference line. The output for von Mises stress and the stress inensity confirmed the former results. Although the exact location of maximum deformation is not in the exact location of maximum deformation is not in the cervical region, due to the reduced thickness of the enamel rods in the CEJ, it shows the disruption of the enamel, thus resulting in the wedge-shape lesions found in this area. Incisal extension of these lesions sould be a support of the comparison of these tesions and the comparison of these tesions found in this area. Incisal extension of these lesions found in this area.

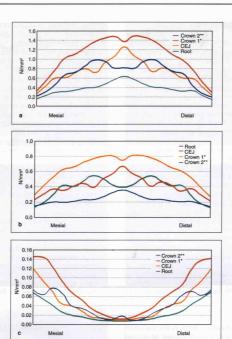


Fig 5 von Mises stress of the cervical area in a mesiodistal direction: (a) Tipping force application (0 degrees); (b) 45-degree force application; (c) intrusive force application (90 degrees). CEJ = cementoenamel junction; * = first crown layer adjacent to the CEJ. ** = second crown layer.

REFERENCES

- Sturdevant CM, Roberson TM, Heymann HO, Sturdevant JR. The Art and Science of Operative Dentistry, ed 3. St Louis: CV Mosby, 1995:2-8.
- Levitch LC, Bader JD, Shugars DA, Heymann HO. Noncarious cervical lesions. J Dent 1994;22(4):195–207.
- Osborne-Smith KL, Burke FJ, Wilson NH. The etiology of the non-carious cervical lesions. Am J Dent 1999;12: 283-285.
- Rees JS. The role of cuspal flexure in the development of abfraction lesion, a finite element study. Eur J Oral Sci 1998;106:1028-1032.
- Schwartz RS, Summitt JB, Robins JW. Fundamentals of Operative Dentistry. Chicago: Quintessence, 1996:309.

- Addy M, Embery G. Tooth Wear and Sensitivity: Clinical Advances in Restorative Dentistry. London: Martin Dunitz, 2000:90.
- Grippo JO. Abfraction: A new classification of hard tissue lesion of the teeth. J Esthet Dent 1991;3:14–19.
- 8. Xhonga FA. Bruxism and its effect on the teeth. J Oral Rehabil 1977;4:65-76.
- Burke FJT, Whitehead SA, McCaughey AD. Contemporary concepts in the pathogenesis of the class V non-carious lesion. Dent Update 1995;22:28–32.
- Lee CW, Eakle WS. Stress-induced cervical lesions: Review of advances in the past 10 years. J Prosthet Dent 1996;75: 487, 404
- Zienkiewicz OC, Taylor RL. The Finite Element Method. London: McGraw-Hill, 1989.

532 Volume 34, Number 7, 2003

- Geramy A. Moment/force ratio and the centre of rotation: 3D analysis by means of the finite element method. J Dent, Shiraz University of Medical Sciences 2000;1:26-34.
- Geramy A. Alveolar bone resorption and the center of resistance modification (3-D analysis by means of the finite element method). Am J Orthod Dent Orthop 2000;117: 399-405.
- Geramy A. Initial stress produced in the periodontal membrane by orthodontic loads in the presence of varying loss of alveolar bone: A three-dimensional finite element analysis. Eur J Orthod 2002;24:21–33.
- Geramy A. The cervical headgear force system: 3D analysis by means of the finite element method. J Dent, Shiraz University of Medical Sciences 2000;2(3):21-30.
- Brackett WW, Browning WD, Ross JA, Gregory PN, Owens BM. 1-year clinical evaluation of compo glass and Fuji II LC in cervical erosive/abfraction lesions. Am J Dent 1999; 12:119-122.
- Brackett WW, Browning WD, Ross JA, Brackett MG. Twoyear clinical performance of a polyacid-modified resin composite and a resin-modified glass-ionomer restorative material. Oper Dent 2001;26:12–16.
- Brackett WW, Gilpatrick RO, Browning WD, Gregory PN. Two-year clinical performance of a resin-modified glassionomer restorative material. Oper Dent 1999;24:3-9.
- Folwaczny M, Mehl A, Kunzelmann KH, Hickel R. Clinical performance of a resin-modified glass-iconomer and a compomer in restoring non-carious cervical lesions: 5 year results. Am J Dent 2001;14:153–156.
- Tay FR, Kwong SM, Itthagarun A, King NM, Yip Hik, Moulding KM, Pashley DH. Bonding of a self-etching primer to non-carious cervical sclerotic dentin: Interfacial ultra structure and micro tensile bond strength evaluation. J Adhes Dent 2000:29-29.
- Tay MJ, Burrow MF. Clinical evaluation of a resin-modified glass-ionomer adhesive system—Results at three years. Oper Dent 2001;26:17–20.
- Swift EJ Jr, Perdigao J, Heymann HO, et al. Eighteen-month clinical evaluation of a filled and unfilled dentin adhesive. J Dent 2001:29:1–6.
- Kowng SM, Tay FR, Yip HK, Kei LH, Pashley DH. An ultra structure study of the application of dentin adhesives to acid-conditioned sclerotic dentine. J Dent 2001;28:515–528.
- Burrow MF, Tyas MJ. 1-year clinical evaluation of one-step in non-carious cervical lesions. Am J Dent 1999;12: 283-285.
- VanDijken JW. Clinical evaluation of three adhesive systems in class V non-carious lesions. Dent Mater 2000;16: 285-291.
- Brunton PA, Cowan AJ, Wilson NH. A three-year evaluation of restorations placed with a smear-layer mediated dentin-bonding agent in non-carious cervical lesions. J Adhes Dent 1999;1:333-341.
- Bader JD, McClure F, Scurria MS, Shugars DA, Heymann HO. Case-control study of non-carious cervical lesions. Community Dent Oral Epidemiol 1996;24:286–291.

- Levitch LC, Bader JD, Shugars DA, Heymann HO. Noncarious cervical lesions. J Dent 1994;22:195-207.
- Tyas MJ. The class V lesions: Etiology and restoration. Aust Dent J 1995;40:167–170.
- Osborne-Smith KL, Burke FJ, Wilson NH. The etiology of the non-carious cervical lesions. Int Dent J 1999;49:139–143.
- Palamara D, Palamara JE, Tyas MJ, Messer HH. Strain patterns in cervical enamel of teeth subjected to occlusal loading. Dent Mater 2000;16:412-419.
- Khan F, Young WG, Shahabi S, Daley TJ. Dental cervical lesions associated with occlusal erosion and attrition. Aust Dent J 1999;44:176–186.
- Ash MM. Dental Anatomy, Physiology and Occlusion, ed 6. Philadelphia: Saunders, 1984:118–129.
- Coolidge ED. The thickness of the human periodontal membrane. J Am Dent Assoc 1937;24:1260-1270.
- Popov EP. Mechanics of Materials, ed 2. Englewood Cliffs, NI: Prentice-Hall, 1976.
- Lee WC, Eakle WS. Possible role of tensile stress in the etiology of cervical erosive lesion of teeth. J Prosthet Dent 1984:52:374-380.
- 37. Lee WC. Readers, round table. J Prosthet Dent 1985;53:600.
- Bowen RL, Rodrigues MS. Tensile strength and modulus of elasticity of tooth structure and several restorative materials.
 J Am Dent Assoc 1962;64:378–387.
- Lambrechts P, Braem M, Vanherle G. Buonocore memorial lecture. Evaluation of clinical performance for posterior composite resins and dentin adhesives. Oper Dent 1987;12: 53-78.
- Braem M, Lambrechts P, Vanherle G. Stress-induced cervical lesions. J Prosthet Dent 1992;67:718–722.
- Telles D, Pegoraro LF, Pereira JC. Prevalence of noncarious cervical lesions and their relation to occlusal aspects: A clinical study. J Esthet Dent 2000;12:10–15.
- Khera SC, Geol VK, Chen RCS, Gurusami SA. A three dimensional finite element model. J Oper Dent 1988;13: 128-137.
- Kaewsuriyathumrong C, Soma K. Stress of tooth and PDL structure created by bite force. Bull Tokyo Med Dent Univ 1993;40:217–232.
- Takahashi N, Kitagami T, Komori T. Behavior of tooth under various loading conditions with finite element method. J Oral Rehabil 1980;7:453-461.
- Rubin C, Krishnamurthy N, Capilouto E, Yi H. Stress analysis of the human teeth using a three-dimensional finite element model. J Dent Res 1983;62(2):82–86.
- Geol VK, Khera SC, Ralston JL, Chan KH. Stresses at the dentoenamel junction of human teeth. A finite element investigation. J Prosthet Dent 1991;66:451–459.
- Sakaguchi RL, Brust EW, Cross M, Delong R, Douglas WH. Independent movement of cusp during occlusal loading. J Dent Mater 1991;7:186–190.